



# Small Launch Vehicle (SLV) Concept Development for Affordable Multi-Stage Inline Configurations

May 22, 2014

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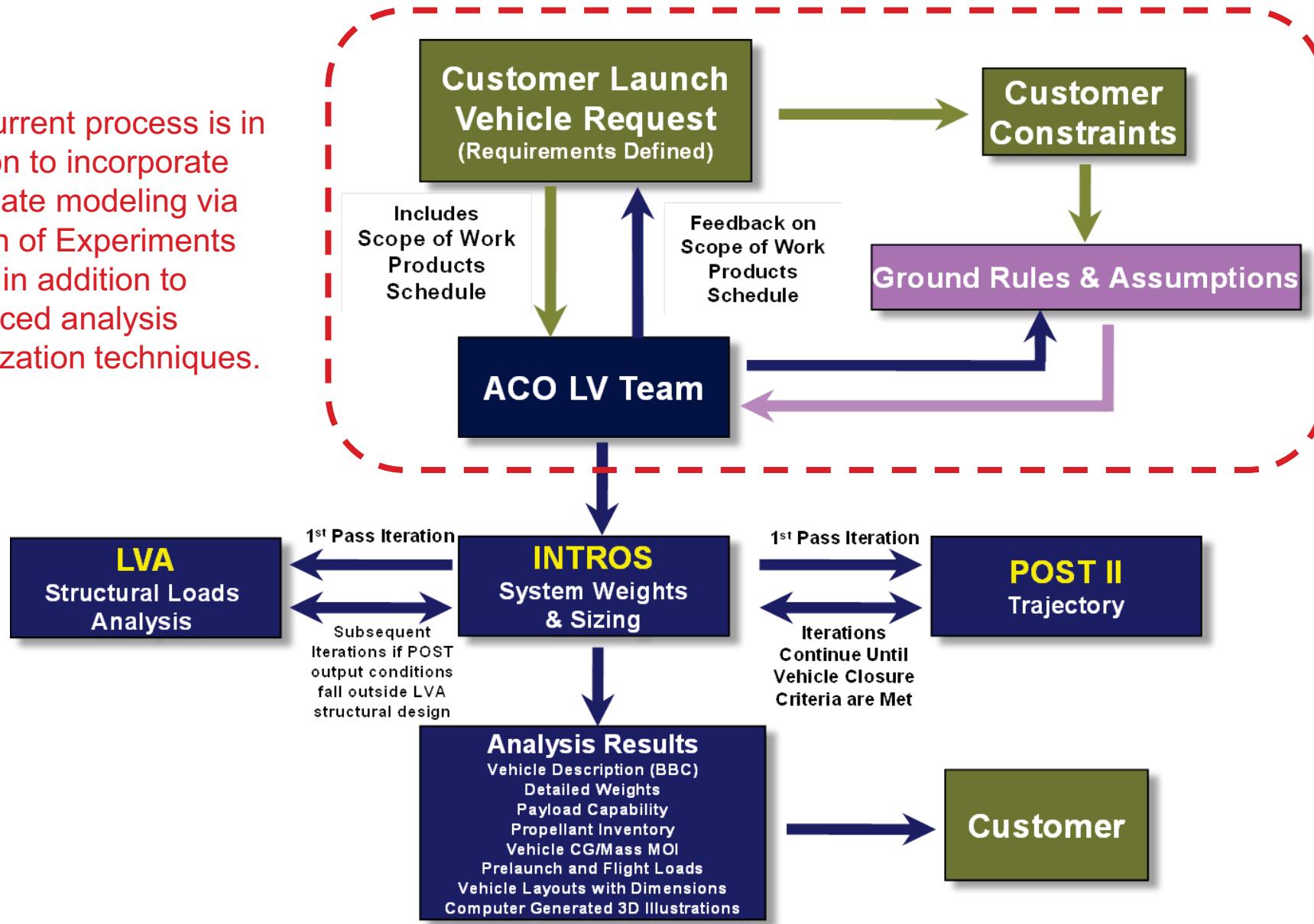
**Ed Threet – Team lead**

*NASA, George C. Marshall Space Flight Center, AL, 35812, United States*

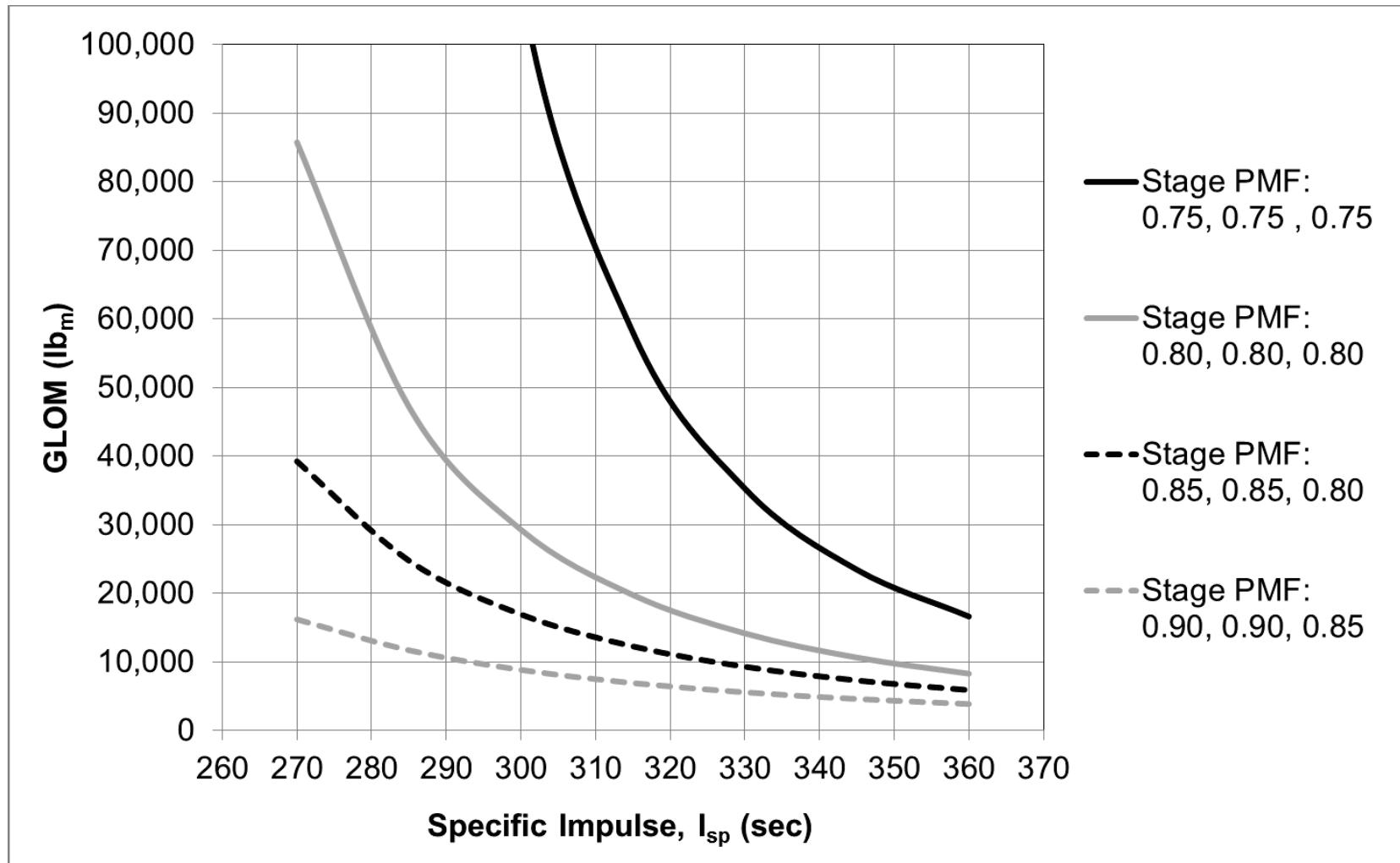


# Earth-To-Orbit Team Process

The current process is in revision to incorporate surrogate modeling via Design of Experiments (DoE) in addition to enhanced analysis visualization techniques.



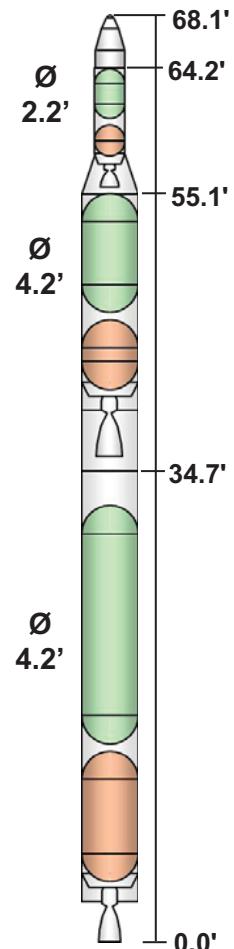
# Generic Trade Space Sizing Tool





# NESC-1 Ground Rules & Assumptions

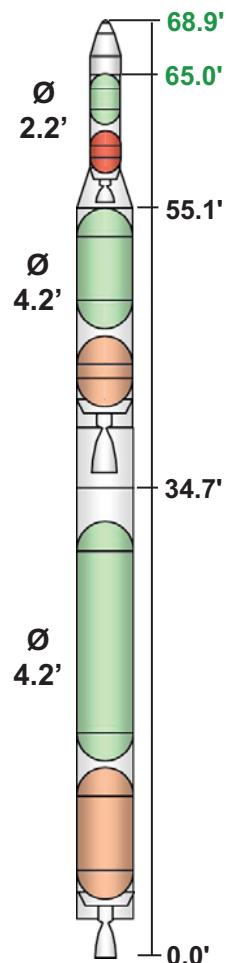
Item	Stage 1	Stage 2	Stage 3
<b>Propulsion</b>			
Propellants	LOX / RP-1	LOX / RP-1	LOX / RP-1
Mixture ratio, MR	2.77	2.77	2.77
Vacuum Thrust (lb <sub>f</sub> )	55,000	18,000	1,000
Vacuum Specific impulse, I <sub>sp</sub> (sec)	300	300	300
Propellant feed system type	Pressure-fed	Pressure-fed	Pressure-fed
Propellant tank pressures (psia)	550	550	250
<b>Structures</b>			
Stage diameter (ft)	4.17	4.17	2.17
Safety factor	1.4	1.4	1.4
Mass growth allowance, MGA (%)	batt, avionics = 25 all other = 18	batt, avionics = 25 all other = 18	batt, avionics = 25 all other = 18
All vehicle structural material	IM7/877	IM7/877	IM7/877
<b>Trajectory</b>			
Orbit type / delivery altitude (nmi)	Circular / 200		
Inclination (deg)	28.5°		
Propellant Mass Fraction (PMF)	0.84	0.83	0.71

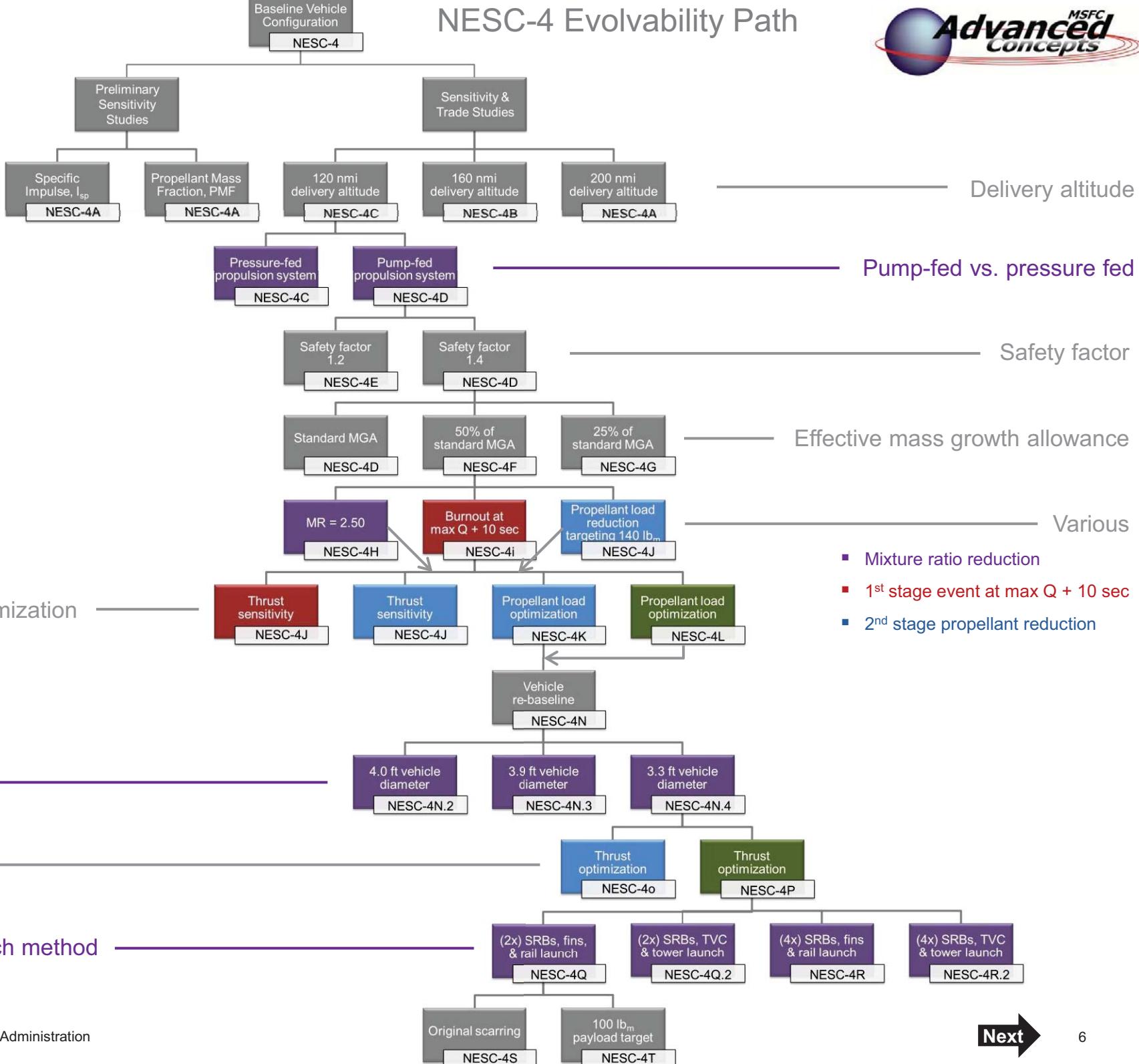
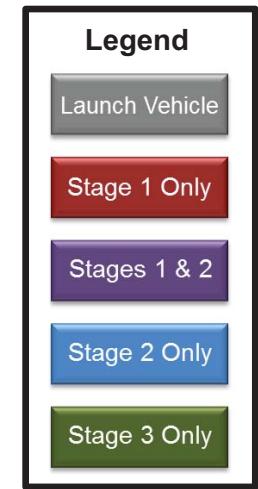




# NESC-4 Ground Rules & Assumptions

Item	Stage 1	Stage 2	Stage 3
<b>Propulsion</b>			
Propellants	LOX / RP-1	LOX / RP-1	LOX / LCH <sub>4</sub>
Mixture ratio, MR	2.77	2.77	3.45
Vacuum Thrust (lb <sub>f</sub> )	55,000	18,000	1,000
Vacuum Specific impulse, I <sub>sp</sub> (sec)	300	300	360
Propellant feed system type	Pressure-fed	Pressure-fed	Pressure-fed
Propellant tank pressures (psia)	550	550	250
<b>Structures</b>			
Stage diameter (ft)	4.17	4.17	2.17
Safety factor	1.4	1.4	1.4
Mass growth allowance, MGA (%)	batt, avionics = 25 all other = 18	batt, avionics = 25 all other = 18	batt, avionics = 25 all other = 18
All vehicle structural material	IM7/877	IM7/877	IM7/877
<b>Trajectory</b>			
Orbit type / delivery altitude (nmi)	Circular / 200		
Inclination (deg)	28.5°		
Propellant Mass Fraction (PMF)	0.84	0.83	0.67

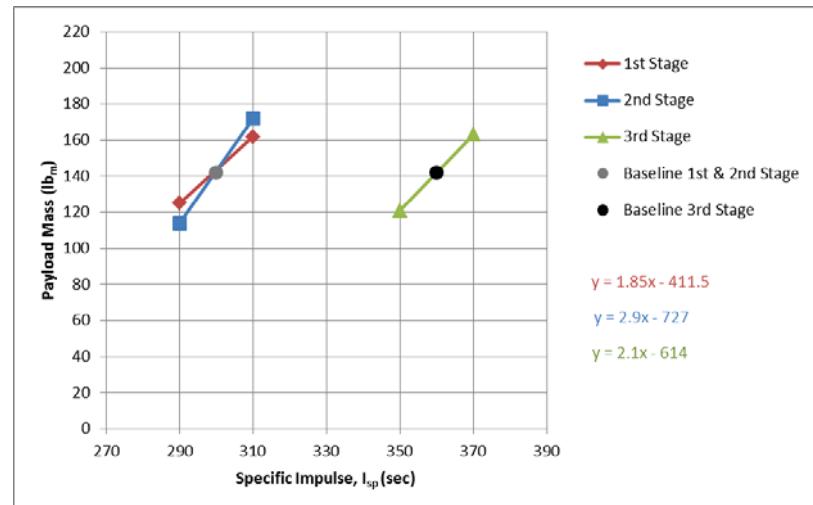
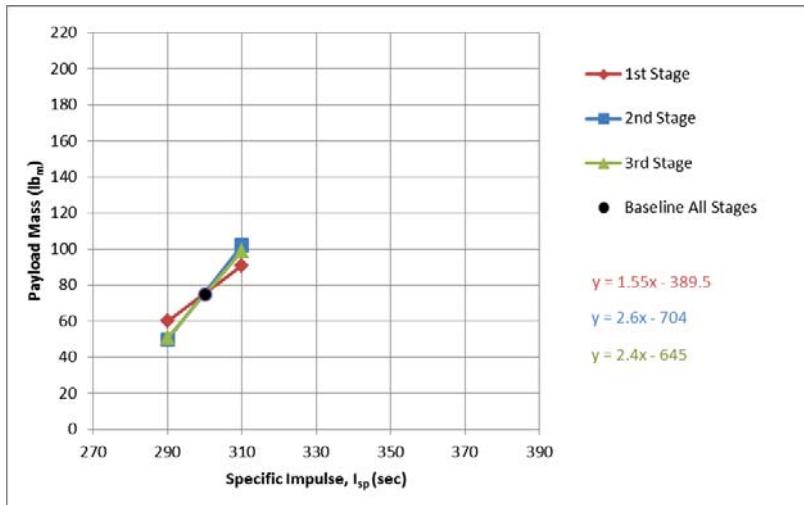




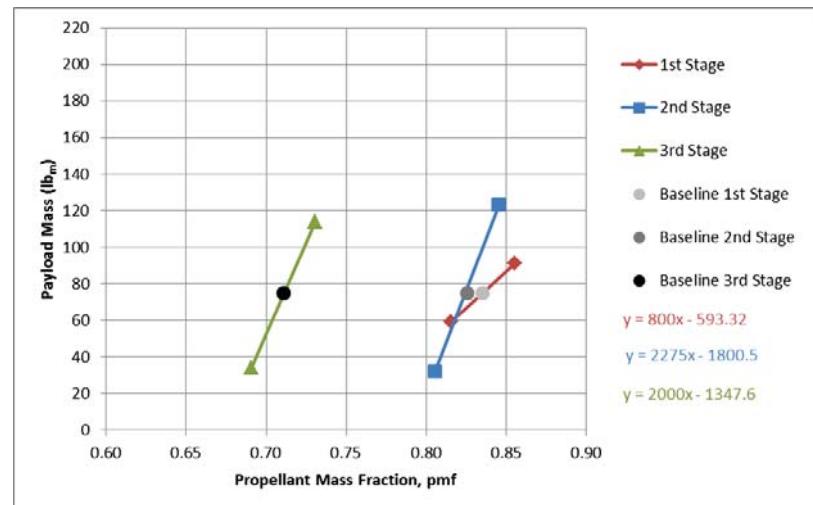
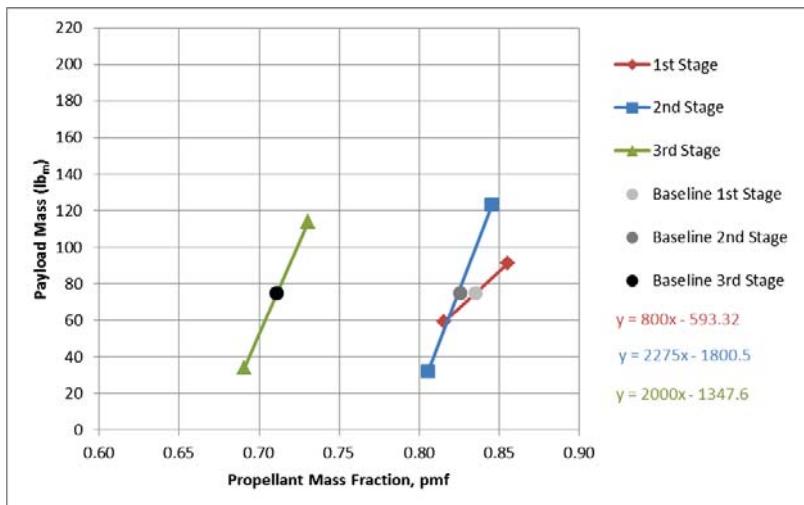


# Preliminary Sensitivity Study Results

## Specific Impulse ( $I_{sp}$ ) Sensitivity



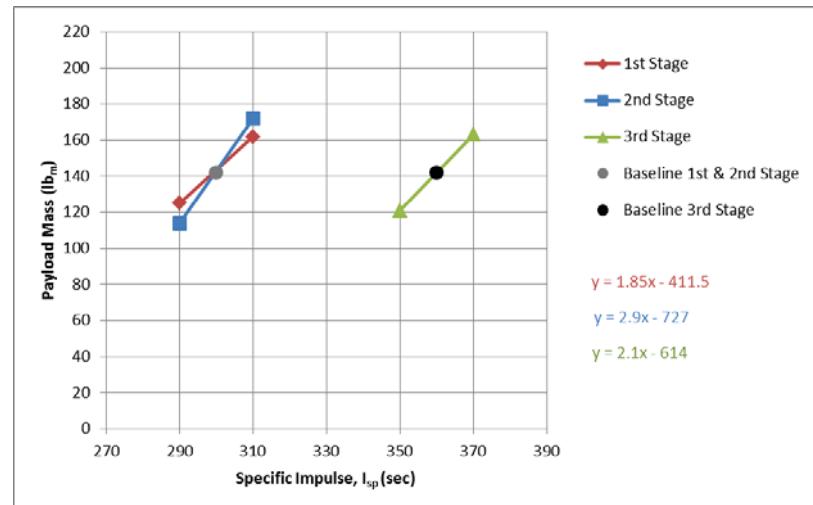
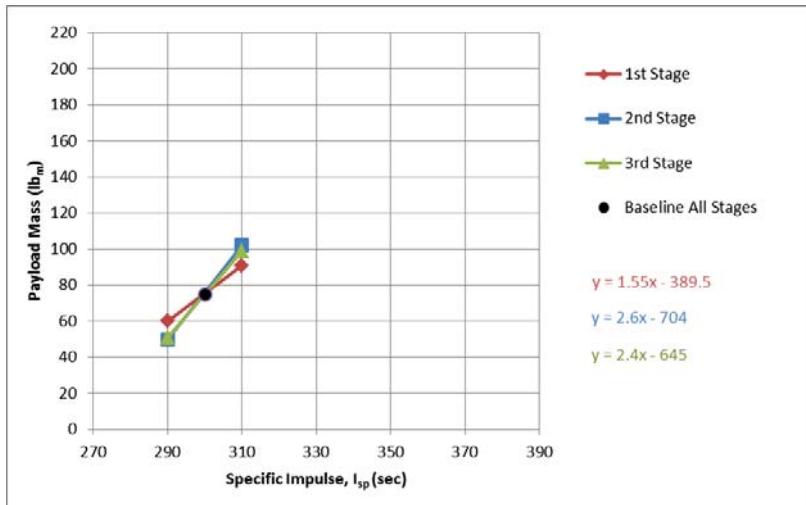
## Propellant Mass Fraction (PMF) Sensitivity



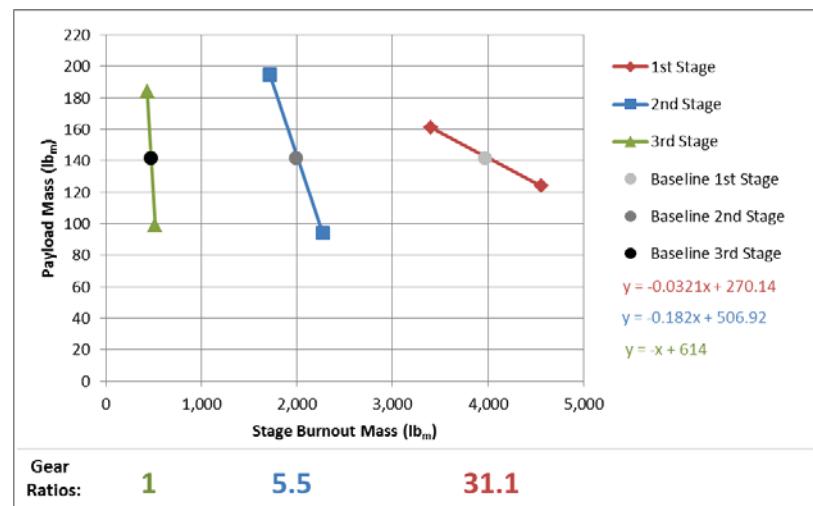
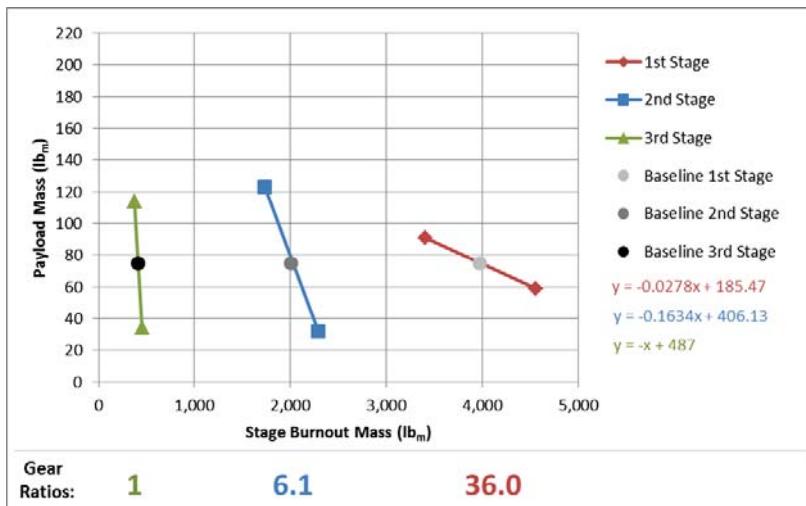


# Preliminary Sensitivity Study Results

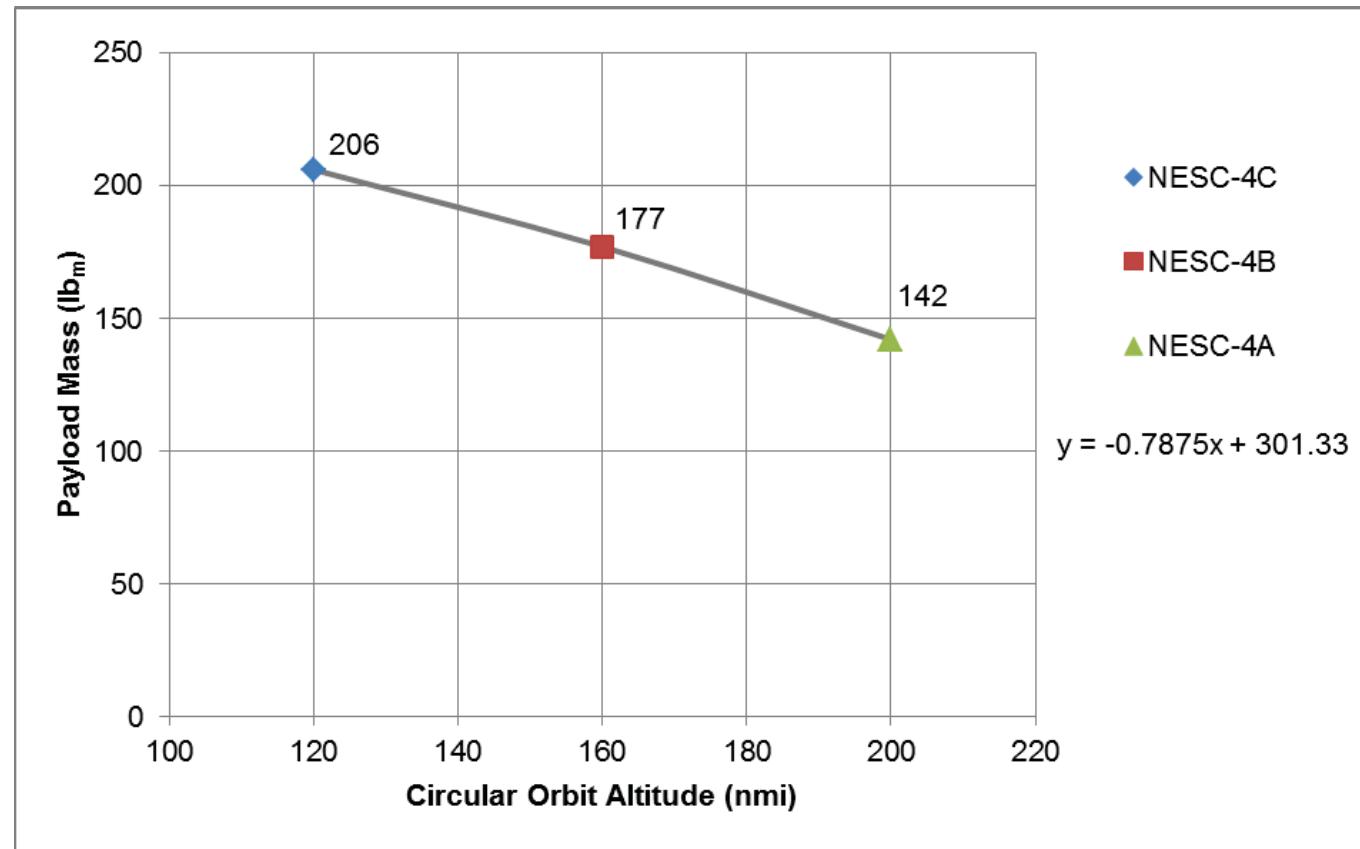
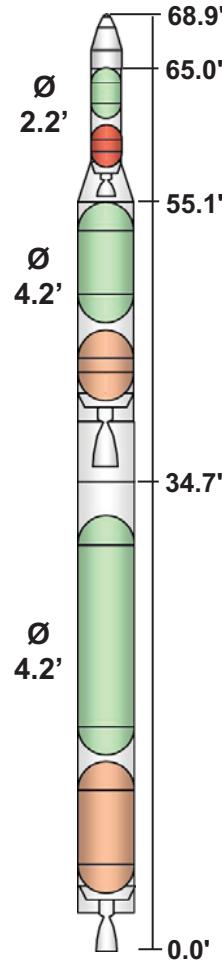
## Specific Impulse ( $I_{sp}$ ) Sensitivity



## Stage Burnout Mass Sensitivity



# Delivery Altitude Sensitivity Study



## Key information:

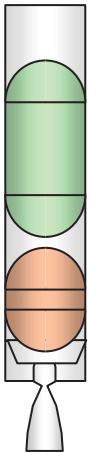
- All vehicles configurations were identical but were flown to different altitudes



# 1st / 2nd Stage Propulsion System Trade Study

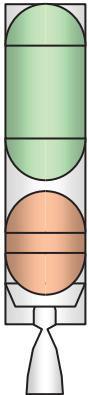


## NESC-4C



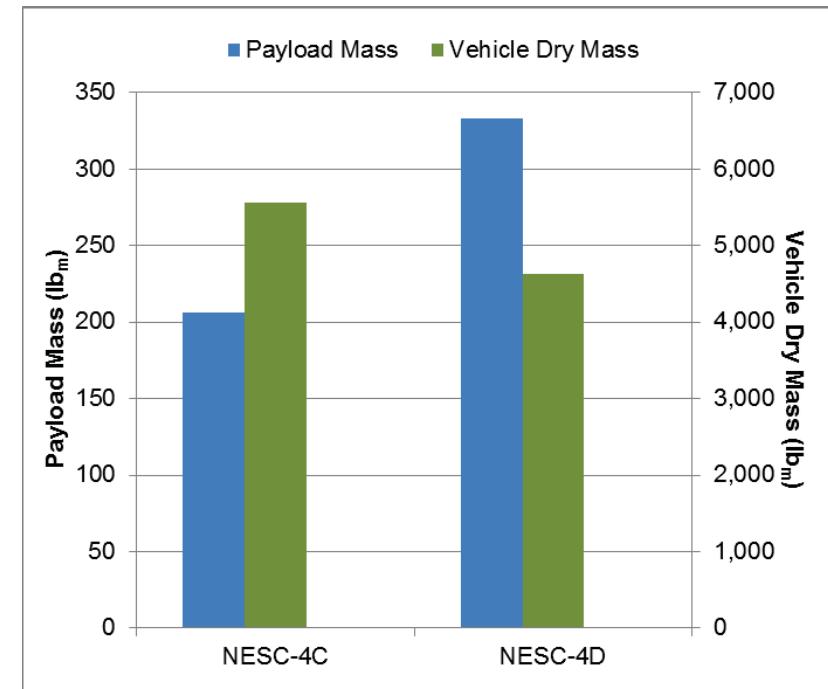
### Pressure-fed system:

- 550 psia tank pressures
- Thick-walled propellant feed system line
- Larger Helium pressurant volume accommodations in forward skirt



### Pump-fed system:

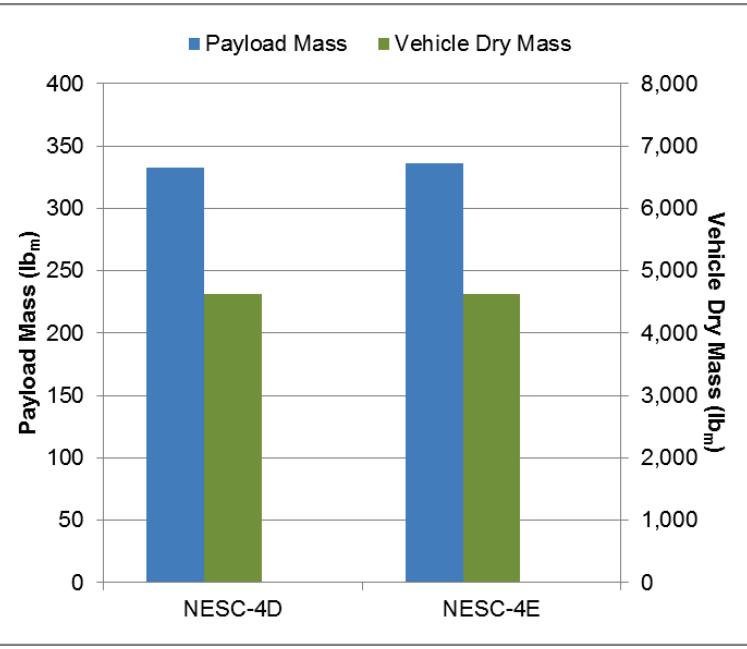
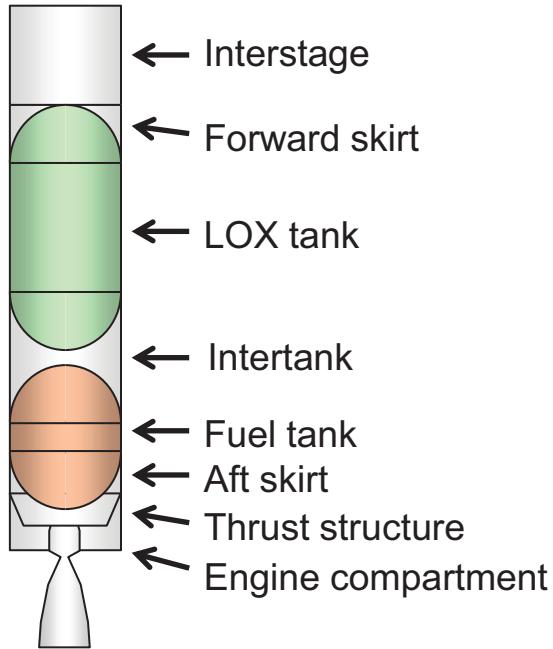
- 50 psia tank pressures
- Thin-walled propellant feed system line
- Smaller Helium pressurant volume accommodations in forward skirt



## NESC-4D



# Vehicle Safety Factor Sensitivity Study

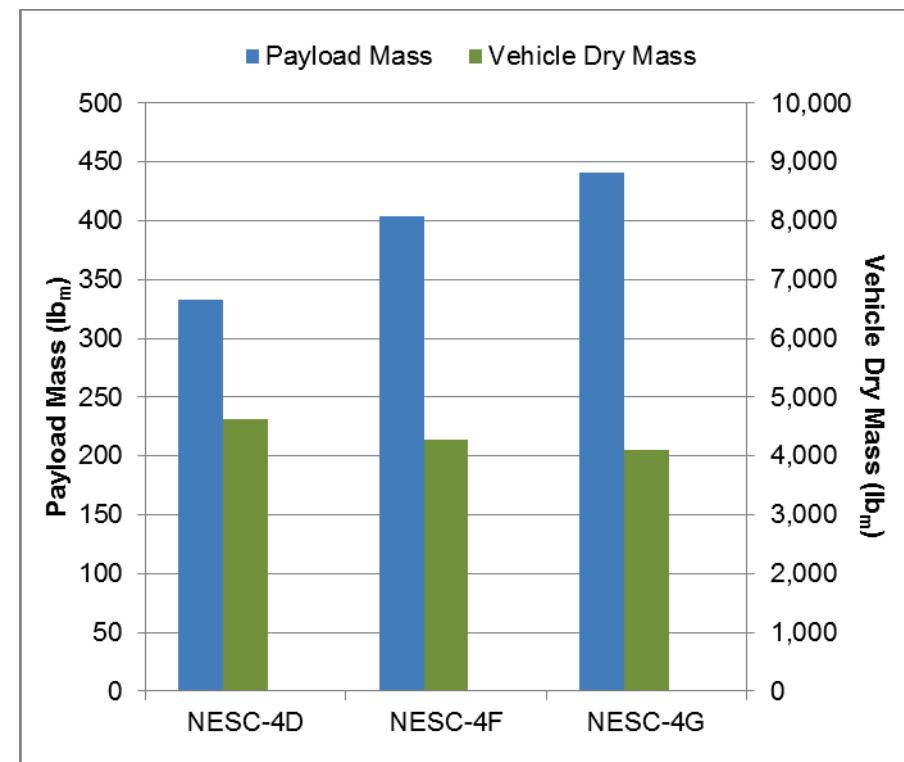
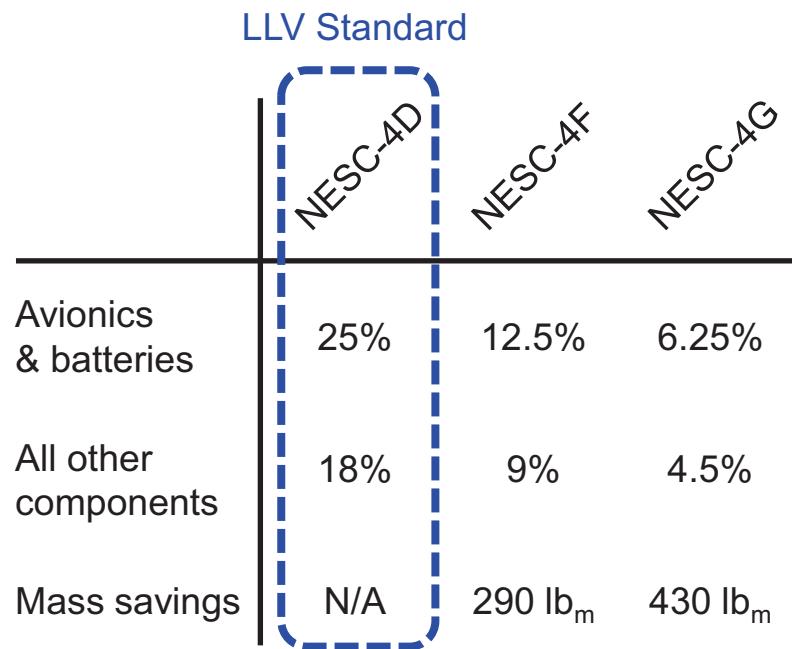


## Key Information:

- IM7/877 graphite epoxy composite ( $\rho = 0.065 \text{ lb}_m/\text{in}^3$ )
- 0.036 in. minimum gauge wall thickness
- 0.65 structural buckling knockdown factor
- 3 $\sigma$  dispersion placed on angle of attack ( $\alpha$ ) calculated by POST
- Combined worst case loading
- 1% risk of exceeding peak prelaunch wind loads at KSC

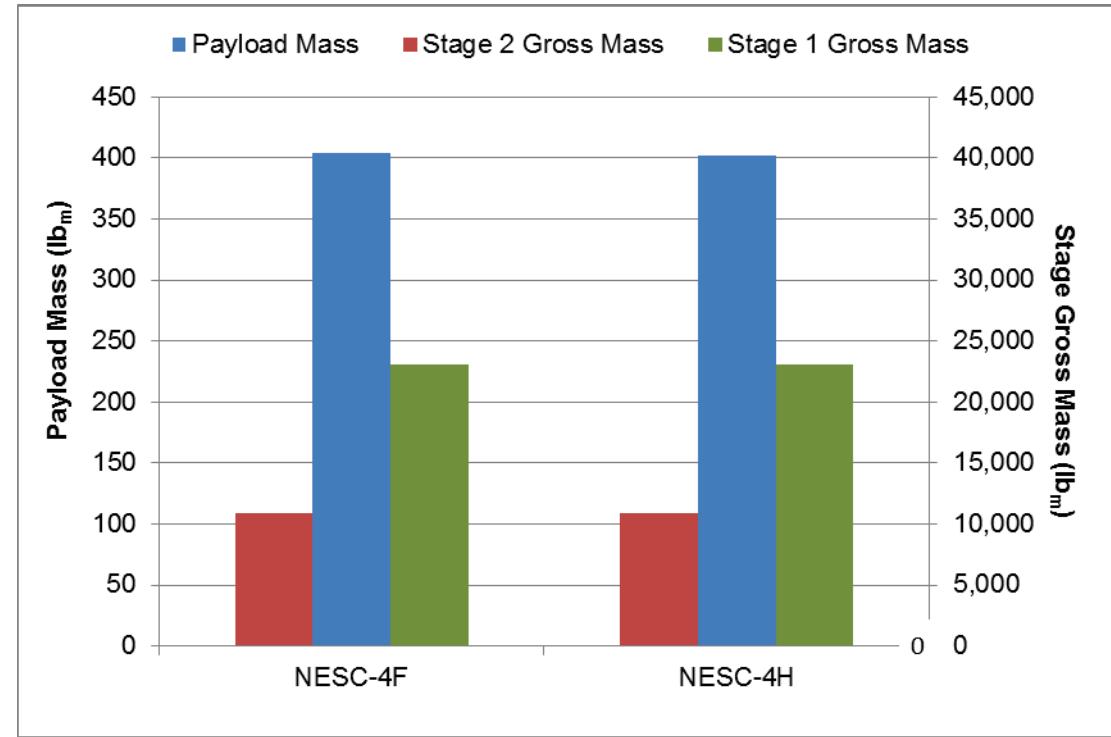
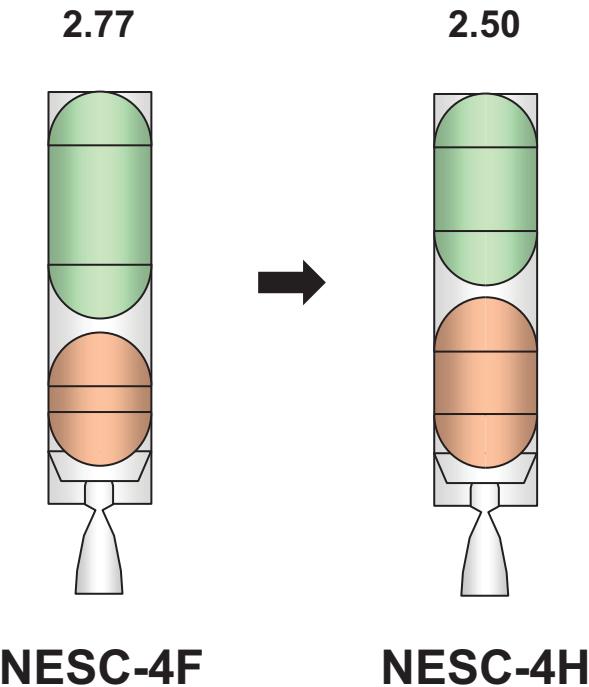


# Vehicle MGA Sensitivity Study





# 1<sup>st</sup> / 2<sup>nd</sup> Stage Mixture Ratio Sensitivity Study

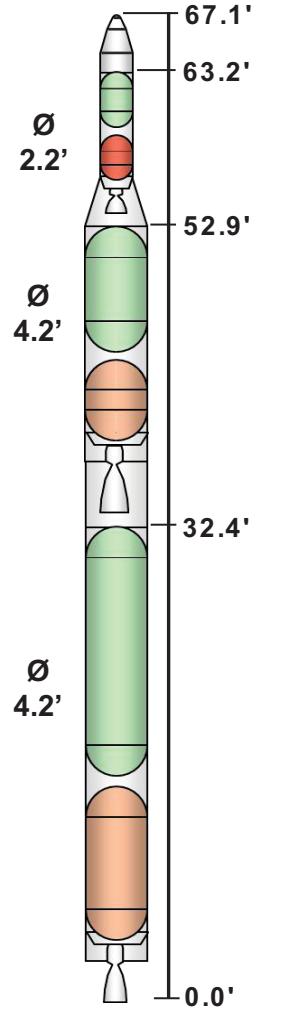


## Key information:

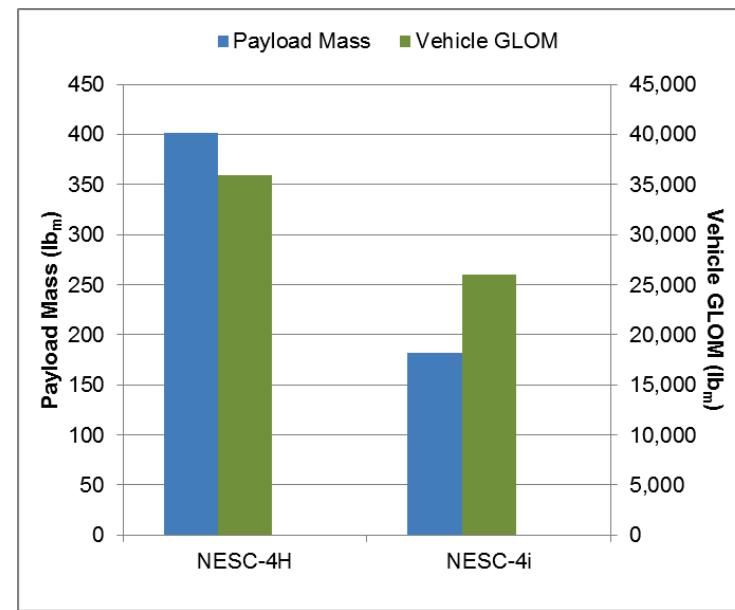
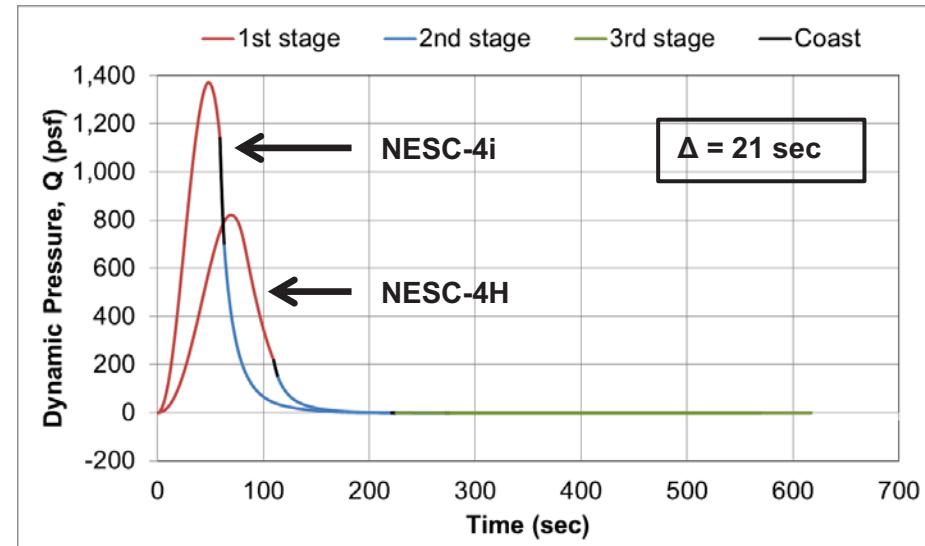
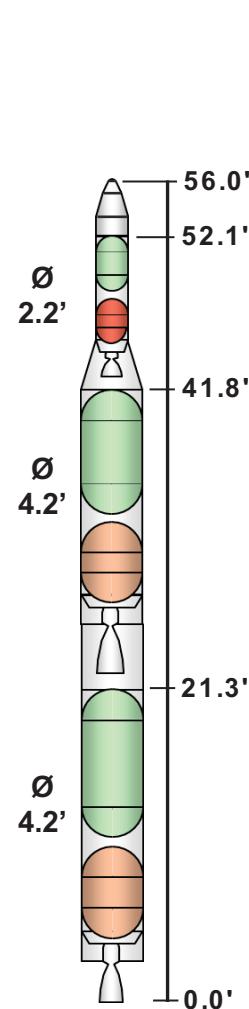
- GLOM was held constant so payload capability was minimally affected.
- MR was adjustable since only conceptual engines were used.

$$MR = \frac{\dot{m}_{oxidizer}}{\dot{m}_{fuel}}$$

# Maximum Q Event Sensitivity Study



**NESC-4i**

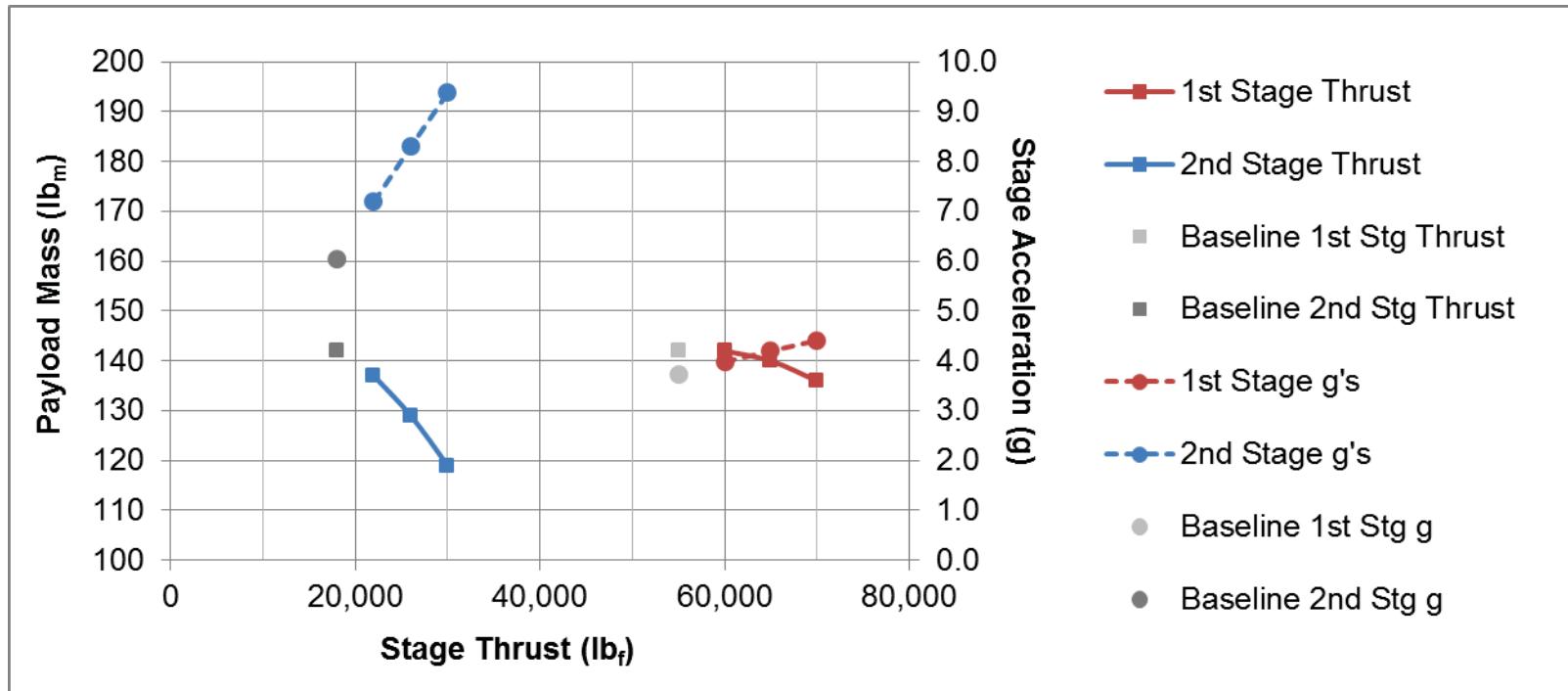


## Key information:

- Propellant was removed only from the 1<sup>st</sup> stage to relocate max Q event in the trajectory.

# 1<sup>st</sup> / 2<sup>nd</sup> Stage Thrust Sensitivity Study

## NESC-4J

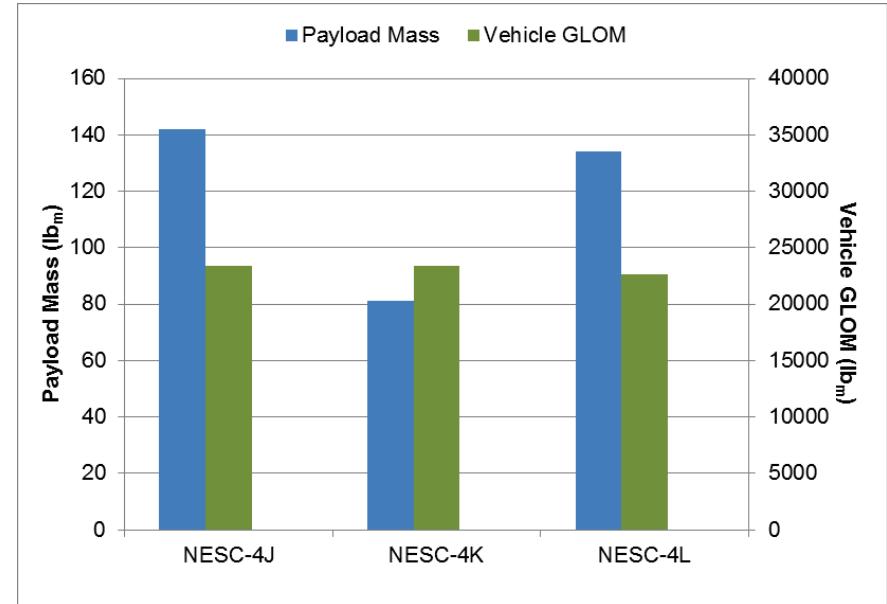
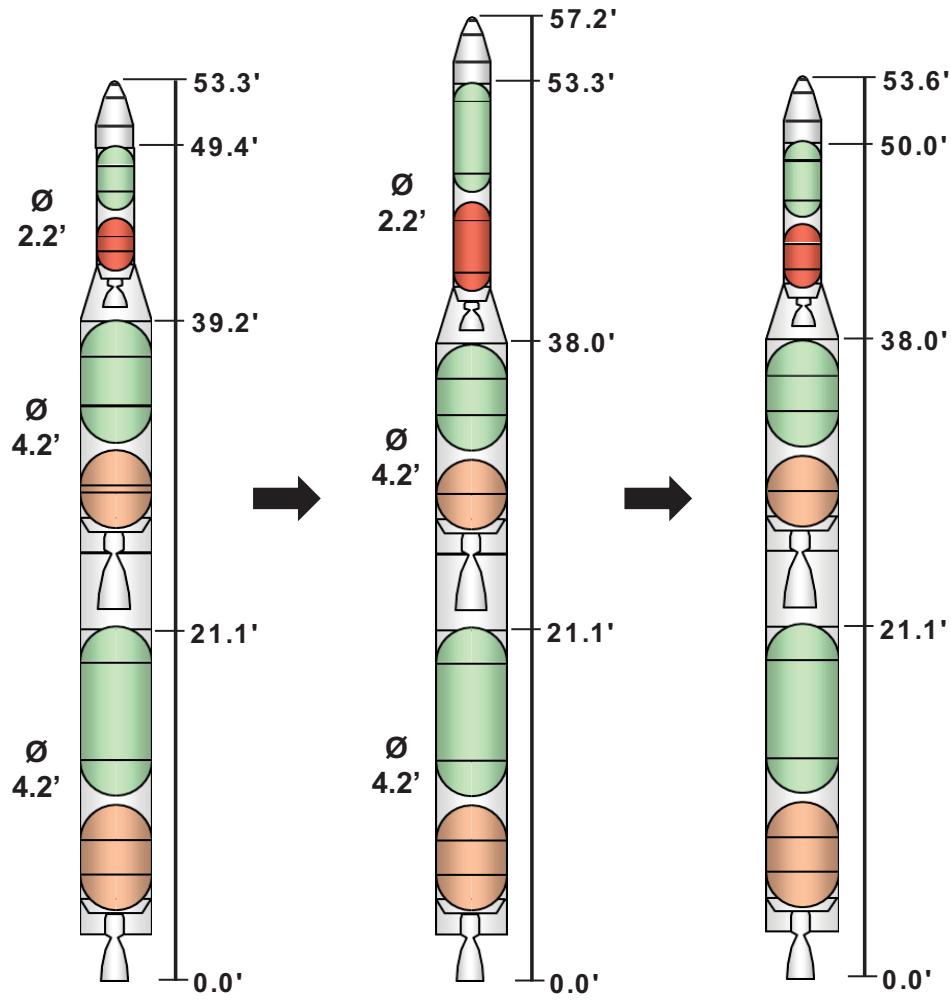


### Key information:

- 55,000  $\text{lb}_f$  (stage 1) and 18,000  $\text{lb}_f$  (stage 2) thrust levels were maintained as result of this sensitivity study.



# 2<sup>nd</sup> / 3<sup>rd</sup> Stage Propellant Load Sensitivity Study



## NESC-4K:

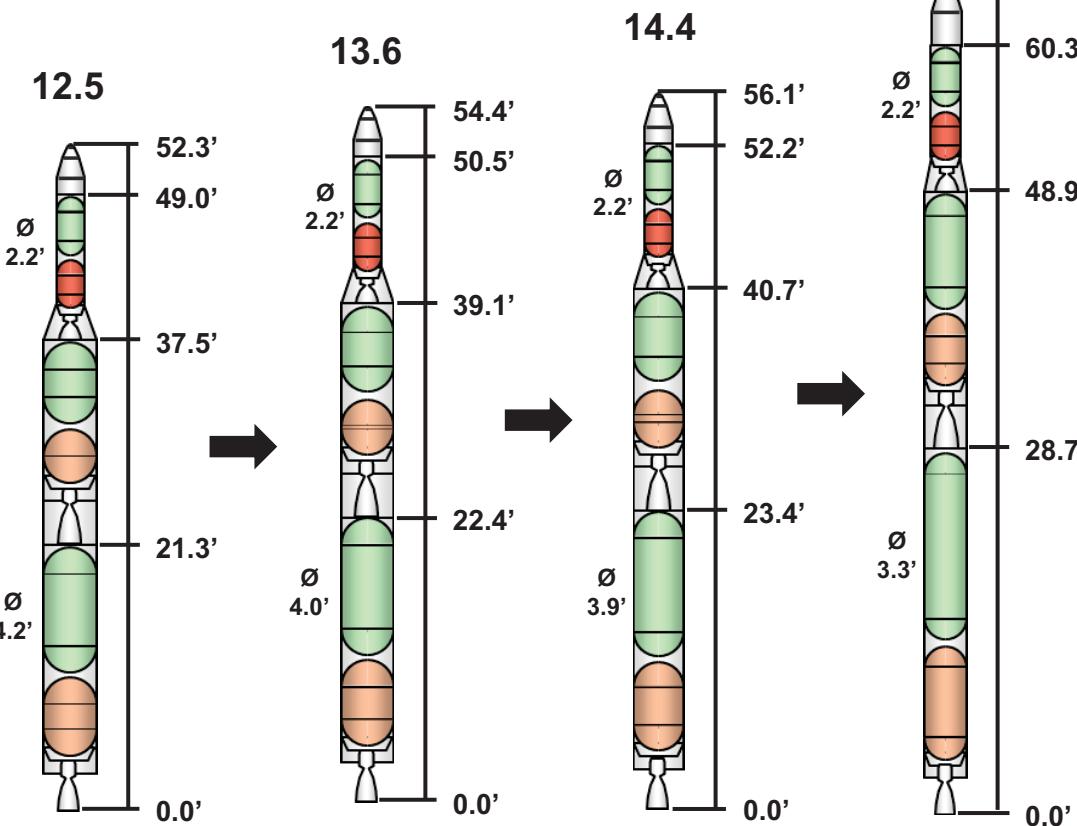
- 2<sup>nd</sup> stage designed such that RP-1 tank was dome-to-dome.
- Equivalent propellant load was placed in 3<sup>rd</sup> stage.

## NESC-4J:

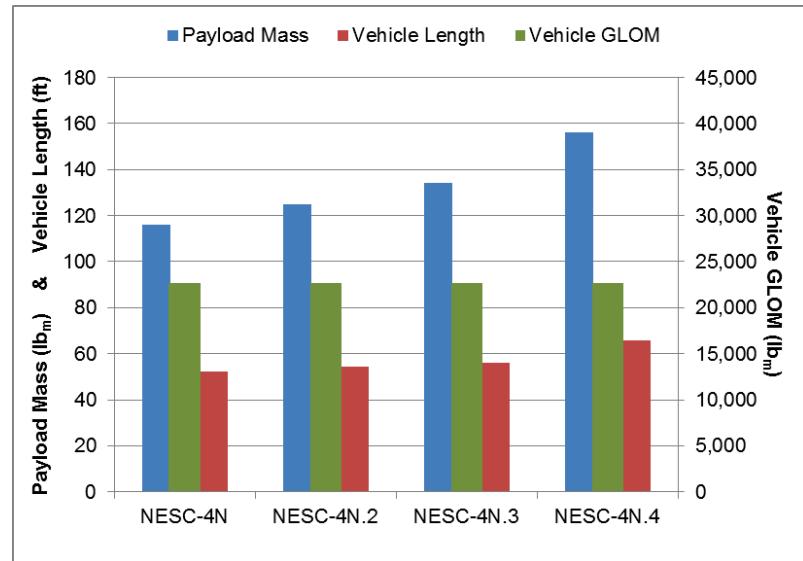
- 3<sup>rd</sup> stage propellant load optimized.

# Vehicle Diameter Sensitivity Study

$$\frac{L}{D} = \frac{\text{Total vehicle length}}{\text{Maximum vehicle diameter}}$$



**NESC-4N    NESC-4N.2    NESC-4N.3    NESC-4N.4**

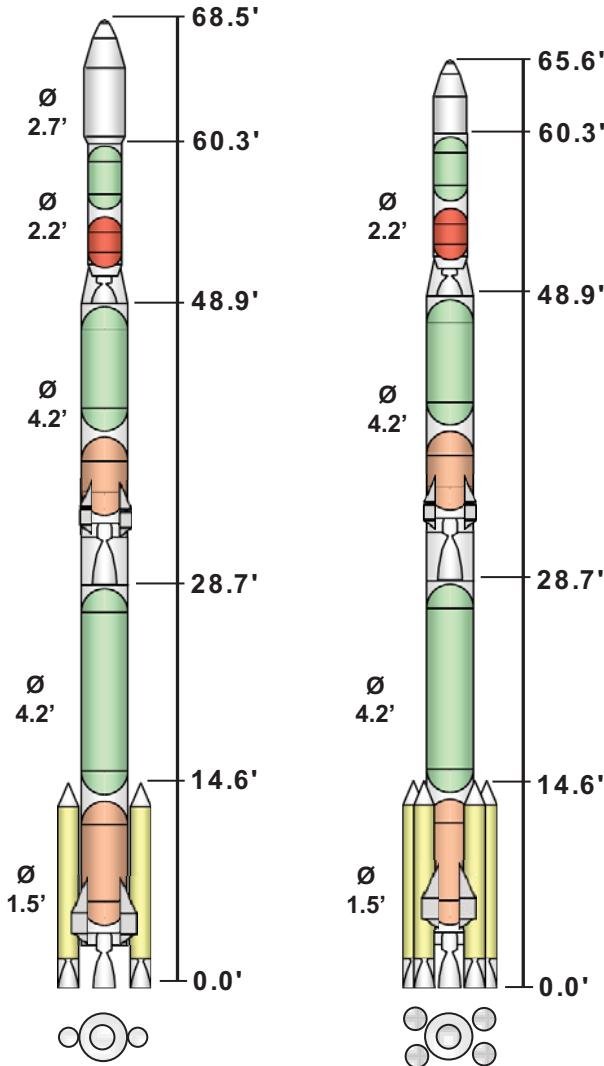


## Key information:

- Vehicle GLOM was maintained such that only stage component geometries were affected.
- Intertank and forward/aft skirts were shortened to accommodate same coverage of propellant tanks as overall dome size shrunk.

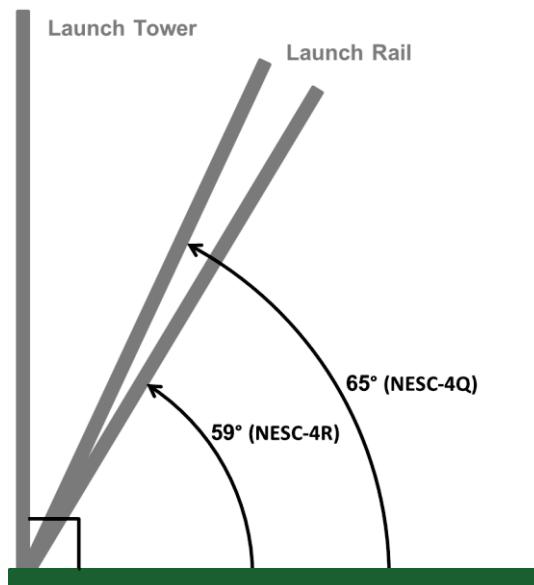
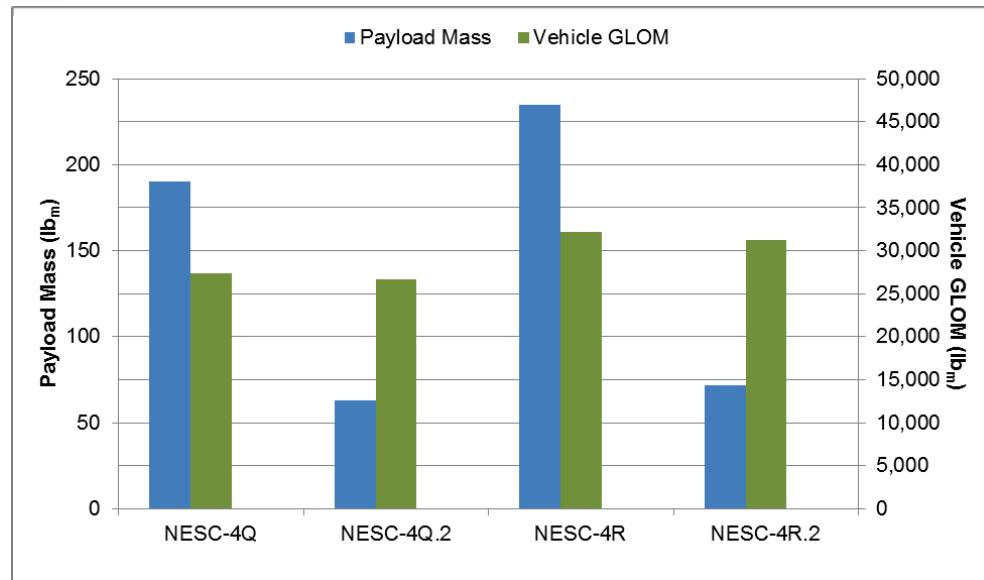


# SRB & Launch Rail Trade Study



**NESC-4Q**

**NESC-4R**



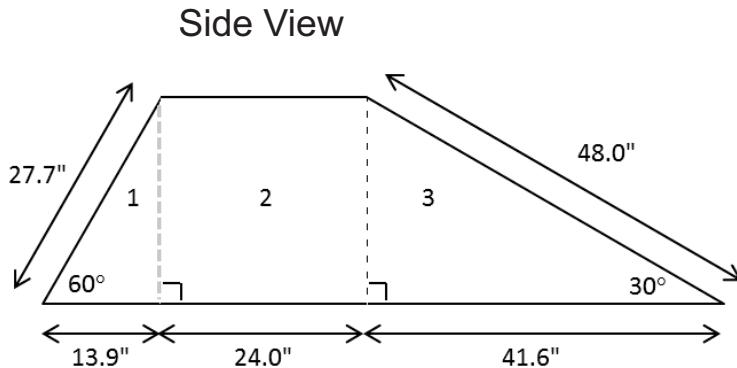
## Key information:

- SRBs (Mk 70 Mod ER) in quantities of 2 and 4 were added to sufficiently increase rail exit velocity.
- 1<sup>st</sup> and 2<sup>nd</sup> stage TVC systems were replaced with groups of 4 fins sized to maintain sufficient stability margin.
- Launch configurations were changed from a 90° tower launch to rail launches, each at their own optimized angles.



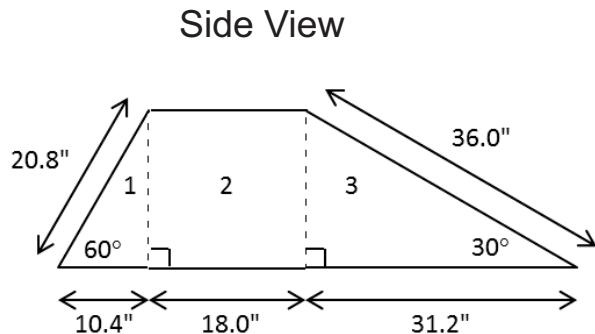
# Passive vs. Active Guidance System

## NESC-4Q – 1<sup>st</sup> stage fin design



Item	Stage 1	Stage 2
<b>NESC-4Q</b>		
Graphite epoxy composite fins	4	4
Surface area per fin (ft <sup>2</sup> )	17.9	10.1
Volume per fin (ft <sup>3</sup> )	0.7	0.4
Mass per fin (lb <sub>m</sub> )	80.7	45.4
Vehicle stability margin	1.72 (SRBs) 2.13 (no SRBs)	1.21

## NESC-4Q – 2<sup>nd</sup> stage fin design



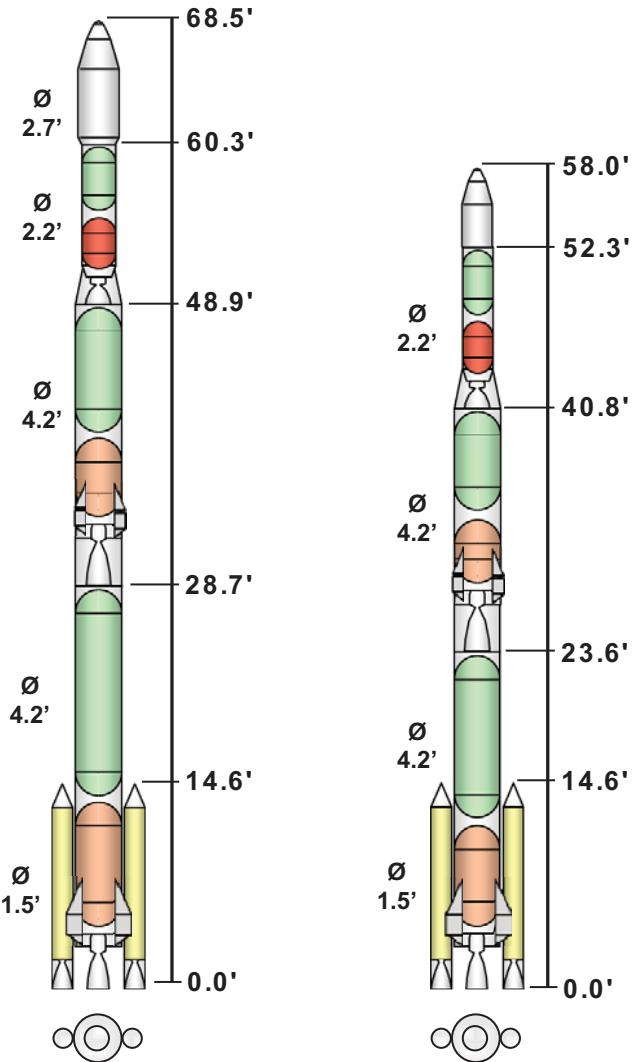
Item	Stage 1	Stage 2
<b>NESC-4R</b>		
Graphite epoxy composite fins	4	4
Surface area per fin (ft <sup>2</sup> )	27.9	10.1
Volume per fin (ft <sup>3</sup> )	1.1	0.4
Mass per fin (lb <sub>m</sub> )	126.0	45.4
Vehicle stability margin	1.64 (SRBs) 3.09 (no SRBs)	1.25

**Note:** Stability margin rule of thumb is for CG to be forward of CP at ignition by:

- 1<sup>st</sup> stage ~ 1.5 – 2.0 vehicle diameters
- Subsequent stages ~ 1.0 vehicle diameters (if low enough in the atmosphere)

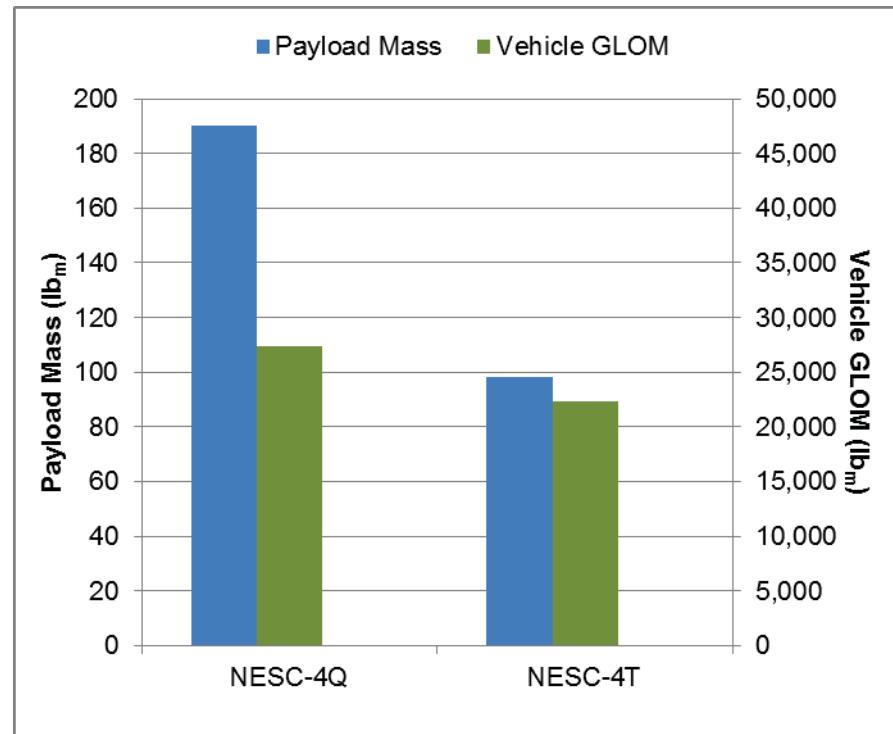


# 100 lb<sub>m</sub> Payload Target



**NESC-4Q**

**NESC-4T**

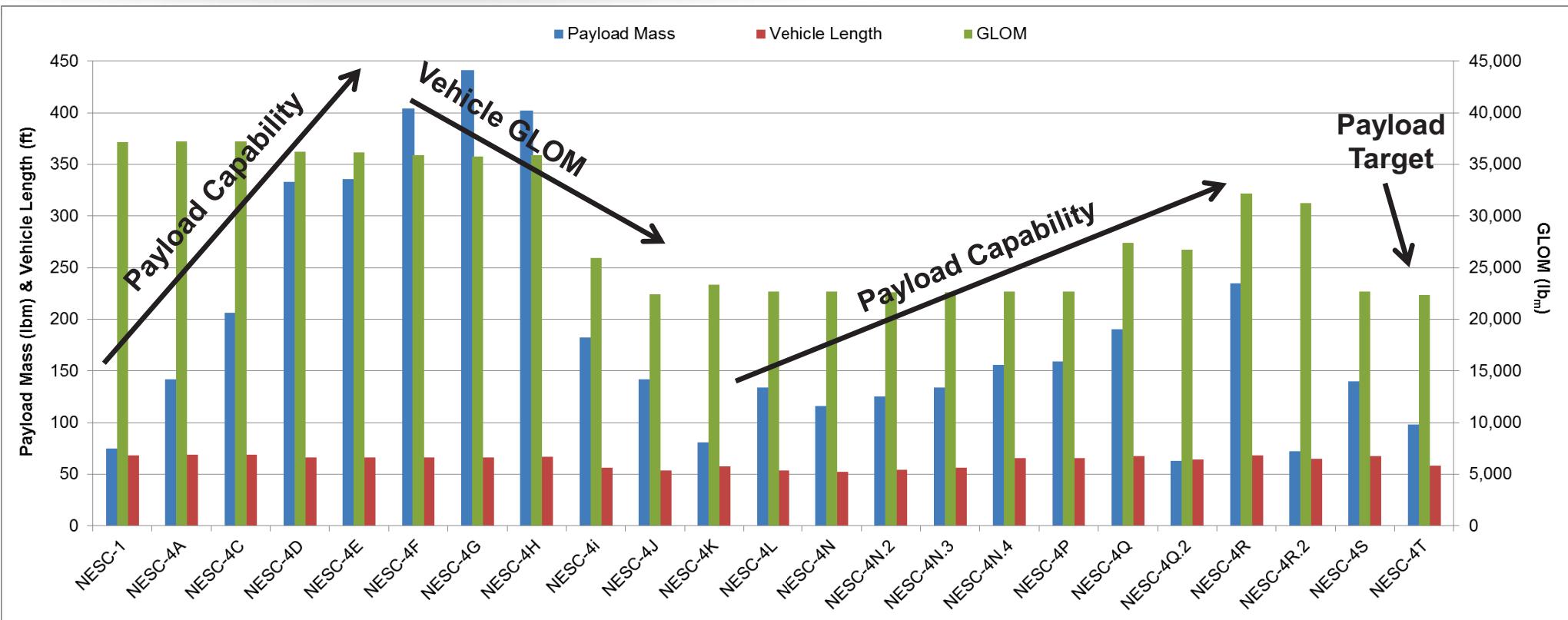


## Key Information:

- Removed propellant from both 1<sup>st</sup> and 2<sup>nd</sup> stages to achieve 100 lb<sub>m</sub> payload target.

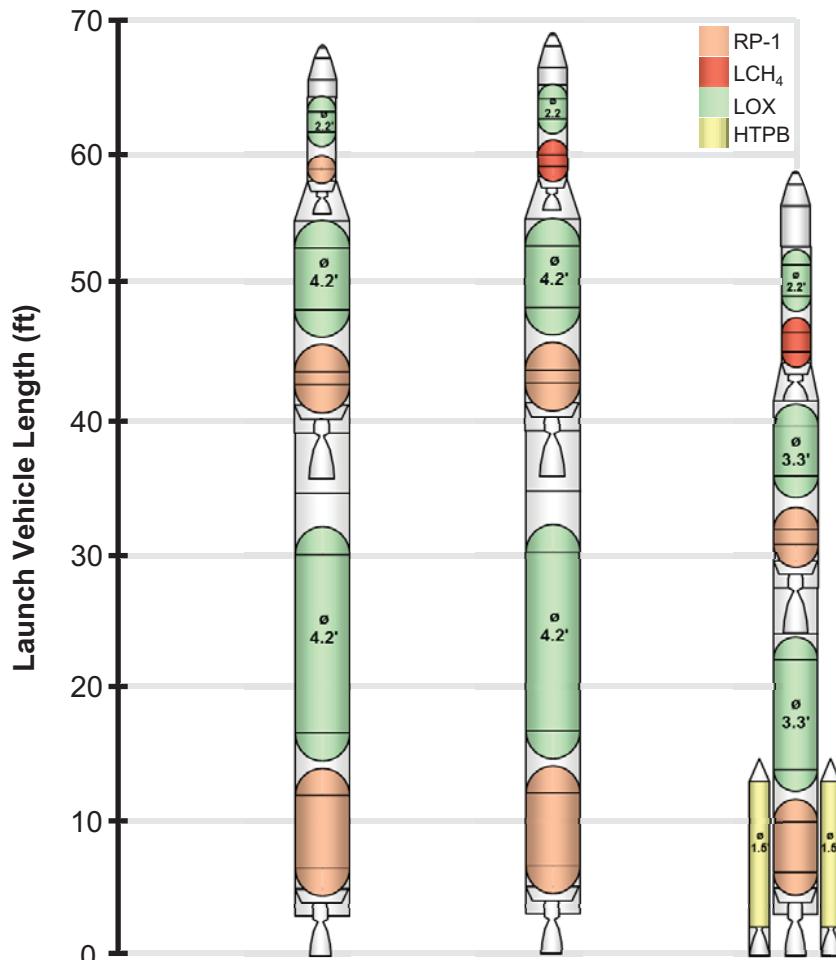


# Results Summary



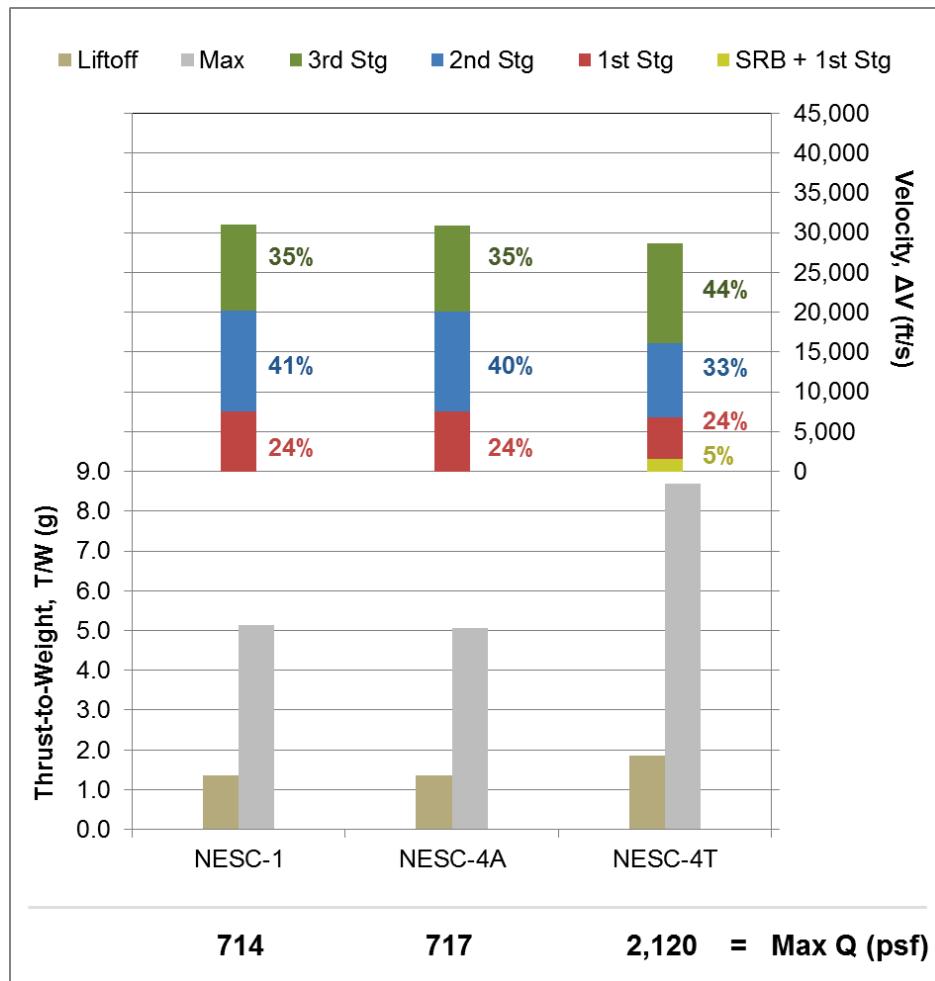
LOX / RP-1	120 nmi circ	SF = 1.2	25% of Standard MGA	1 <sup>st</sup> stage max Q + 10	2 <sup>nd</sup> stage propellant optimization	MER scrub & rebaseline	1 <sup>st</sup> /2 <sup>nd</sup> stage diameter optimization (3.85 ft)	3 <sup>rd</sup> stage thrust optimization	(2x) SRBs with 1 <sup>st</sup> /2 <sup>nd</sup> stage TVC, tower launc	(4x) SRBs with 1 <sup>st</sup> /2 <sup>nd</sup> stage TVC, tower launc	100 lb <sub>m</sub> payload target
3 <sup>rd</sup> stage LOX / LCH <sub>4</sub>	1 <sup>st</sup> /2 <sup>nd</sup> stage pump-fed	50% of Standard MGA	1 <sup>st</sup> /2 <sup>nd</sup> stage MR = 2.50	140 lb <sub>m</sub> payload target	3 <sup>rd</sup> stage propellant optimization	1 <sup>st</sup> /2 <sup>nd</sup> stage diameter optimization (4.0 ft)	1 <sup>st</sup> /2 <sup>nd</sup> stage diameter optimization (3.3 ft)	(2x) SRBs with 1 <sup>st</sup> /2 <sup>nd</sup> stage fins, rail launc	(4x) SRBs with 1 <sup>st</sup> /2 <sup>nd</sup> stage fins, rail launc	Original scarring of NES-4Q.2	

# Bookend Configuration Comparison



Configuration	NESC-1	NESC-4A	NESC-4T
GLOM (lb <sub>m</sub> )	37,133	37,187	22,378
LEO Payload (lb <sub>m</sub> )	75	142	98
Delivery Orbit (nmi)	200 circ	200 circ	120 circ

## Loads & Ideal Velocity ( $\Delta V$ ) Split Results





# BACK-UP



# NESC 1 Sensitivity Study Summary

■ = parent vehicle

↓ / ↑ = with reference to parent vehicle

Group	Sensitivity Study
NESC-1	Baseline ground rules and assumptions
NESC-1	1 <sup>st</sup> stage $I_{sp}$ = +10 sec (310 sec)
NESC-1	1 <sup>st</sup> stage $I_{sp}$ = -10 sec (290 sec)
NESC-1	2 <sup>nd</sup> stage $I_{sp}$ = +10 sec (310 sec)
NESC-1	2 <sup>nd</sup> stage $I_{sp}$ = -10 sec (290 sec)
NESC-1	3 <sup>rd</sup> stage $I_{sp}$ = +10 sec (310 sec)
NESC-1	3 <sup>rd</sup> stage $I_{sp}$ = -10 sec (290 sec)
NESC-1	1 <sup>st</sup> stage PMF = +0.02 (0.8573)
NESC-1	1 <sup>st</sup> stage PMF = -0.02 (0.8171)
NESC-1	2 <sup>nd</sup> stage PMF = +0.02 (0.8480)
NESC-1	2 <sup>nd</sup> stage PMF = -0.02 (0.8078)
NESC-1	3 <sup>rd</sup> stage PMF = +0.02 (0.7308)
NESC-1	3 <sup>rd</sup> stage PMF = -0.02 (0.6908)

GLOM (lb <sub>m</sub> )	Veh. Length (ft)	Payload (lb <sub>m</sub> )
37,133 –	68.1 –	75 –
37,149 ↑	68.1 –	91 ↑
37,118 ↓	68.1 –	60 ↓
37,160 ↑	68.1 –	102 ↑
37,108 ↓	68.1 –	50 ↓
37,157 ↑	68.1 –	99 ↑
37,109 ↓	68.1 –	51 ↓
36,586 ↓	68.1 –	91 ↑
37,707 ↑	68.1 –	59 ↓
36,909 ↓	68.1 –	123 ↑
37,375 ↑	68.1 –	32 ↓
37,134 ↑	68.1 –	114 ↑
37,133 –	68.1 –	34 ↓

NESC-4A	Baseline ground rules and assumptions
NESC-4A	1 <sup>st</sup> stage $I_{sp}$ = +10 sec (310 sec)
NESC-4A	1 <sup>st</sup> stage $I_{sp}$ = -10 sec (290 sec)
NESC-4A	2 <sup>nd</sup> stage $I_{sp}$ = +10 sec (310 sec)
NESC-4A	2 <sup>nd</sup> stage $I_{sp}$ = -10 sec (290 sec)
NESC-4A	3 <sup>rd</sup> stage $I_{sp}$ = +10 sec (370 sec)
NESC-4A	3 <sup>rd</sup> stage $I_{sp}$ = -10 sec (350 sec)

37,187 –	68.9 –	142 –
37,205 ↑	68.9 –	162 ↑
37,170 ↓	68.9 –	125 ↓
37,217 ↑	68.9 –	172 ↑
37,159 ↓	68.9 –	114 ↓
37,209 ↑	68.9 –	163 ↑
37,166 ↓	68.9 –	121 ↓



# NESC 4 Sensitivity Study Summary (cont.)

■ = parent vehicle

Group	Sensitivity Study
NESC-4A	1 <sup>st</sup> stage PMF = +0.02 (0.8573)
NESC-4A	1 <sup>st</sup> stage PMF = -0.02 (0.8171)
NESC-4A	2 <sup>nd</sup> stage PMF = +0.02 (0.8494)
NESC-4A	2 <sup>nd</sup> stage PMF = -0.02 (0.8093)
NESC-4A	3 <sup>rd</sup> stage PMF = +0.02 (0.6897)
NESC-4A	3 <sup>rd</sup> stage PMF = -0.02 (0.6497)
NESC-4B	160 nmi circular orbit altitude
NESC-4C	120 nmi circular orbit altitude
NESC-4D	1 <sup>st</sup> and 2 <sup>nd</sup> stage pump-fed propulsion systems
NESC-4E	Vehicle structural safety factor = 1.2
NESC-4F	50% MGA allowable (12.5% batt, avionics; 9% all other)
NESC-4G	25% MGA allowable (6.25% batt, avionics; 4.5% all other)
NESC-4H	1 <sup>st</sup> and 2 <sup>nd</sup> stage LOX / RP-1 MR = 2.50
NESC-4i	1 <sup>st</sup> stage propellant reduction for burnout at max Q +10 sec
NESC-4J	2 <sup>nd</sup> stage propellant reduction targeting 140 lb <sub>m</sub> payload
NESC-4J	2 <sup>nd</sup> stage thrust = +4,000 lb <sub>f</sub> (22 klb <sub>f</sub> )
NESC-4J	2 <sup>nd</sup> stage thrust = +8,000 lb <sub>f</sub> (26 klb <sub>f</sub> )
NESC-4J	2 <sup>nd</sup> stage thrust = +12,000 lb <sub>f</sub> (30 klb <sub>f</sub> )
NESC-4J	1 <sup>st</sup> stage thrust = +5,000 lb <sub>f</sub> (60 klb <sub>f</sub> )
NESC-4J	1 <sup>st</sup> stage thrust = +10,000 lb <sub>f</sub> (65 klb <sub>f</sub> )
NESC-4J	1 <sup>st</sup> stage thrust = +15,000 lb <sub>f</sub> (70 klb <sub>f</sub> )

↓ / ↑ = with reference to parent vehicle

GLOM (lb <sub>m</sub> )	Veh. Length (ft)	Payload (lb <sub>m</sub> )
36,644 ↓	68.9	161 ↑
37,758 ↑	68.9	124 ↓
36,971 ↓	68.9	195 ↑
37,421 ↑	68.9	94 ↓
37,188 ↑	68.9	184 ↑
37,187 —	68.9	99 ↓
37,223 ↑	68.9	177 ↑
37,252 ↑	68.9	206 ↑
36,196 ↓	66.4 ↓	333 ↑
36,189 ↓	66.4 —	336 ↑
35,907 ↓	66.4 —	404 ↑
35,764 ↓	66.4 —	441 ↑
35,918 ↑	67.1 ↑	402 ↓
25,966 ↓	56.0 ↓	182 ↓
22,436 ↓	53.3 ↓	142 ↓
23,516 ↑	53.3 —	137 ↓
23,585 ↑	53.3 —	129 ↓
23,651 ↑	53.3 —	119 ↓
23,470 ↑	53.3 —	142 —
23,504 ↑	53.3 —	140 ↓
23,538 ↑	53.3 —	136 ↓





# NESC 4 Sensitivity Study Summary (cont.)

■ = parent vehicle



Group	Sensitivity Study
NESC-4K	2 <sup>nd</sup> stage RP-1 tank dome-to-dome, propellant moved to 3 <sup>rd</sup> stage
NESC-4L	3 <sup>rd</sup> stage propellant load (and payload) optimization
NESC-4N	MERs scrubbed and model rebaslined
NESC-4N	1 <sup>st</sup> and 2 <sup>nd</sup> stage vehicle diameter = -0.17 ft (4.0 ft)
NESC-4N	1 <sup>st</sup> and 2 <sup>nd</sup> stage vehicle diameter = -0.32 ft (3.85 ft)
NESC-4N	1 <sup>st</sup> and 2 <sup>nd</sup> stage vehicle diameter = -0.87 ft (3.30 ft)
NESC-4o	2 <sup>nd</sup> stage thrust = -2,000 lb <sub>f</sub> (16 klb <sub>f</sub> )
NESC-4o	2 <sup>nd</sup> stage thrust = -4,000 lb <sub>f</sub> (14 klb <sub>f</sub> )
NESC-4o	2 <sup>nd</sup> stage thrust = +2,000 lb <sub>f</sub> (20 klb <sub>f</sub> )
NESC-4P	3 <sup>rd</sup> stage thrust = +200 lb <sub>f</sub> (1.2 klb <sub>f</sub> )
NESC-4Q	+2 SRBs, 1 <sup>st</sup> /2 <sup>nd</sup> stage passive guidance systems, rail launch
NESC-4Q.2	+2 SRBs, 1 <sup>st</sup> /2 <sup>nd</sup> stage active guidance systems, tower launch
NESC-4R	+4 SRBs, 1 <sup>st</sup> /2 <sup>nd</sup> stage passive guidance systems, rail launch
NESC-4R.2	+4 SRBs, 1 <sup>st</sup> /2 <sup>nd</sup> stage active guidance systems, tower launch
NESC-4S	Original scarring of NESC-4Q.2
NESC-4T	100 lb <sub>m</sub> payload target

↓ / ↑ = with reference to parent vehicle

GLOM (lb <sub>m</sub> )	Veh. Length (ft)	Payload (lb <sub>m</sub> )
23,352 ↑	57.2 ↑	81 ↓
22,675 ↓	53.6 ↓	134 ↑
22,672 ↓	52.3 ↓	116 ↓
22,647 ↓	54.4 ↑	125 ↑
22,634 ↓	56.1 ↑	134 ↑
22,656 ↓	65.6 ↑	156 ↑
22,614 ↓	65.6 –	154 ↓
22,562 ↓	65.6 –	148 ↓
22,703 ↑	65.6 –	154 ↓
22,674 ↑	65.6 –	159 ↑
27,417 ↑	67.8 ↑	190 ↑
26,718 ↑	64.1 ↓	63 ↓
32,169 ↑	68.3 ↑	235 ↑
31,275 ↑	64.9 ↓	72 ↓
22,675 ↓	67.8 ↑	140 ↑
22,378 ↓	58.0 ↓	98 ↓

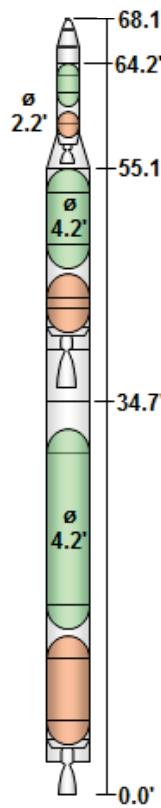


NESC-4Q



# NESC-1 (baseline)

<u>Interstage</u>	
Second/Third	
Dry Mass	33 lbm
<u>Third Stage</u>	
Propellants	LOX / Jet-A
Nominal Ascent Propellant	1,012 lbm
Stage pmf	0.7108
Dry Mass	360 lbm
Burnout Mass	412 lbm
# Engines	1
Engine Thrust (100.0%)	1,000 lbf @ Vac
Engine Isp (100.0%)	300.0 sec @ Vac
Stage Burn Time	303.9 sec
<u>Delivery Orbit</u>	
LEO Delivery	200.0 x 200.0 nmi @ 28.5°
LEO Gross Payload	75 lbm (34.0 kg)
Insertion Altitude	200.0 nmi
T/W @ Liftoff	1.37
Max Dynamic Pressure	714 psf
Max g's Ascent Burn	5.14
T/W @ 2nd Stage Ignition	1.34
T/W @ 3rd Stage Ignition	0.67



**GLOM** 37,133 lbm  
Shroud Jettison Mass 47 lbm

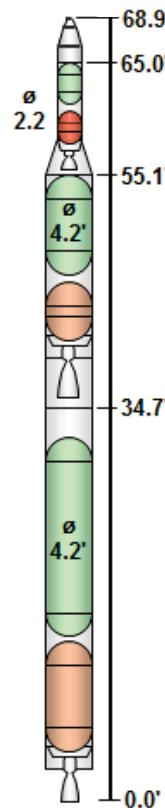
<u>First Stage</u>	
Propellants	LOX / Jet-A
Total Stage Ascent Propellant	20,133 lbm
Stage pmf	0.8372
Dry Mass	3,448 lbm
Burnout Mass	3,915 lbm
# Engines	1
Engine Thrust (100.0%)	55,000 lbf @ Vac
Engine Isp (100.0%)	300.0 sec @ Vac
Mission Power Level	100.0%
Stage Burn Time	109.8 sec
<u>Interstage</u>	
Dry Mass	52 lbm

<u>Second Stage</u>	
Propellants	LOX / Jet-A
Nominal Ascent Propellant	9,482 lbm
Stage pmf	0.8279
Dry Mass	1,720 lbm
Burnout Mass	1,971 lbm
# Engines	1
Engine Thrust (100.0%)	18,000 lbf @ Vac
Engine Isp (100.0%)	300.0 sec @ Vac
Stage Burn Time	158.0 sec



# NESC-4A (baseline)

<u>Interstage</u>	
Second/Third	
Dry Mass	35 lbm
<u>Third Stage</u>	
Propellants	LOX / LCH4
Nominal Ascent Propellant	957 lbm
Stage pmf	0.6697
Dry Mass	420 lbm
Burnout Mass	472 lbm
# Engines	1
Engine Thrust (100.0%)	1,000 lbf @ Vac
Engine Isp (100.0%)	360.0 sec @ Vac
Stage Burn Time	344.5 sec
<u>Delivery Orbit</u>	
LEO Delivery	200.0 x 200.0 nmi @ 28.5°
LEO Gross Payload	142 lbm (64.5 kg)
Insertion Altitude	200.0 nmi
T/W @ Liftoff	1.36
Max Dynamic Pressure	717 psf
Max g's Ascent Burn	5.06
T/W @ 2nd Stage Ignition	1.33
T/W @ 3rd Stage Ignition	0.64



GLOM **37,187 lbm**  
Shroud Jettison Mass 48 lbm

First Stage  
Propellants LOX / Jet-A  
Nominal Ascent Propellant 20,133 lbm  
Stage pmf 0.8372  
Dry Mass 3,448 lbm  
Burnout Mass 3,916 lbm  
# Engines 1  
Engine Thrust (100.0%) 55,000 lbf @ Vac  
Engine Isp (100.0%) 300.0 sec @ Vac  
Mission Power Level 100.0%  
Stage Burn Time 109.8 sec

Interstage First/Second  
Dry Mass 52 lbm

Second Stage  
Propellants LOX / Jet-A  
Nominal Ascent Propellant 9,482 lbm  
Stage pmf 0.8293  
Dry Mass 1,700 lbm  
Burnout Mass 1,952 lbm  
# Engines 1  
Engine Thrust (100.0%) 18,000 lbf @ Vac  
Engine Isp (100.0%) 300.0 sec @ Vac  
Stage Burn Time 158.0 sec



## NESC-4T (100 lb<sub>m</sub> target)

<u>Third Stage</u>		<u>GLOM</u>	22,378 lbm
Propellants	LOX / LCH <sub>4</sub>	Shroud Jettison Mass	88 lbm
Nominal Ascent Propellant	1,227 lbm		
Stage pmf	0.6986	<u>First Stage</u>	
Dry Mass	447 lbm	Propellants	LOX / Jet-A
Burnout Mass	529 lbm	Nominal Ascent Propellant	8,060 lbm
# Engines	1	Stage pmf	0.7953
Engine Thrust (100.0%)	1,200 lbf @ Vac	Dry Mass	1,935 lbm
Engine Isp (100.0%)	360.0 sec @ Vac	Burnout Mass	2,075 lbm
Stage Burn Time	368.0 sec	# Engines	1
<b>Solid Booster (each)</b>		Engine Thrust (100.0%)	45,700 lbf @ Vac
Casing Type	Mk 70 Mod 1 ER	Engine Isp (100.0%)	300.0 sec @ Vac
Propellants	Expendable	Mission Power Level	100.0%
Overboard Propellant	HTPB	Stage Burn Time	52.9 sec
Stage pmf	2,986 lbm	<u>Interstage</u>	First/Second
Burnout mass	0.7042	Dry Mass	43 lbm
# Boosters	1,274 lbm		
Average Thrust @ 70 °F	2	<u>Second Stage</u>	
Stage Burn Time	62,800 lbf	Propellants	LOX / Jet-A
	6.05 sec	Nominal Ascent Propellant	4,916 lbm
<b>Delivery Orbit</b>		Stage pmf	0.8238
LEO Delivery	120.0 x 120.0 nmi @ 28.5°	Dry Mass	959 lbm
LEO Gross Payload	98 lbm (44.5 kg)	Burnout Mass	1,051 lbm
Insertion Altitude	120.0 nmi	# Engines	1
T/W @ Liftoff	1.85	Engine Thrust (100.0%)	14,350 lbf @ Vac
Max Dynamic Pressure	2,120 psf	Engine Isp (100.0%)	300.0 sec @ Vac
Max g's Ascent Burn	8.68	Stage Burn Time	102.8 sec
T/W after SRB separation	1.91	<u>Interstage</u>	Second/Third
T/W @ 2nd Stage Ignition	1.67	Dry Mass	29 lbm
T/W @ 3rd Stage Ignition	0.62		

